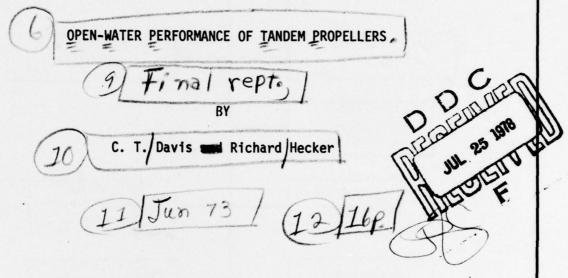




# DAVID W. TAYLOR NAVAL SHIP RESEARCH AND DEVELOPMENT CENTER



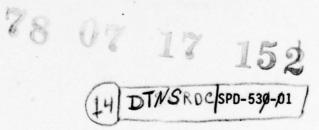
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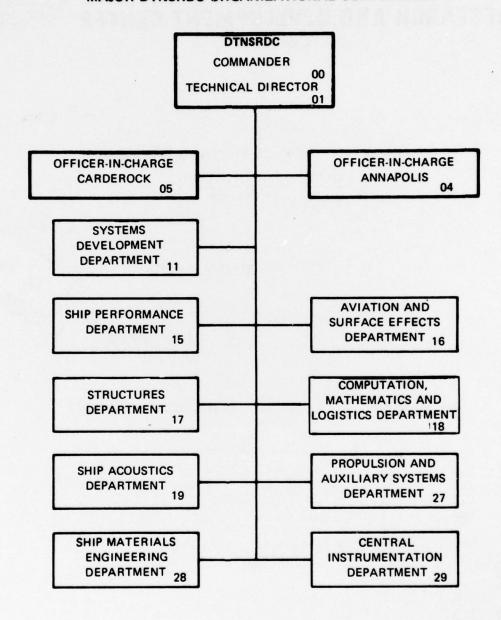
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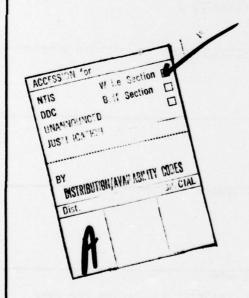
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parent propeller. The performance shows that improved efficiency is obtainable with tandem propellers. The results also show that changes in performance occur with different angular positions of the propellers. Additional experiments are recommended.



### INTRODUCTION

The tandem propellers described in this report consist of two propellers operating one behind the other, on the same shaft with the same rotational speed and direction of rotation. The proper design of such propellers requires special consideration of the distance between forward and after propellers, relative angular position of the blades of the two propellers, and an accurate prediction of the interaction between the two propellers in order that the prescribed loading may be attained. Drawings of one set of tandem propellers (4148 and 4149) designed at the Naval Ship Research and Development Center (NSRDC) are shown in Figures 1 and 2.

The concept of tandem propellers is being explored in an attempt to determine if greater propeller efficiency  $(n_0)$  can be obtained (than for a single propeller) while maintaining the same thrust coefficient  $(K_T)$ . Also, the possibilities exist for reducing blade cavitation by increasing the effective total blade area and/or reducing the loading on each propeller. Other advantages are potential reductions in propeller induced hull and machinery vibrations. Preliminary (unreported) experiments with propellers 4148 and 4149 showed a greater efficiency than was predicted, thus meriting further investigation into their capabilities. This report presents an open water evaluation of these propellers, and compares their performance to the parent propeller, NSRDC propeller 4118.

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### ADMINISTRATIVE INFORMATION

This work was sponsored by Naval Ship Research and Development Center (NSRDC), funded by IR, IED, and performed under Work Unit Number 1528-024.

### PROCEDURE

Open water experiments were conducted at NSRDC on Propellers 4148 and 4149 in April 1973, utilizing Carriage I, the propeller boat, and a 100 inch-pound transmission type dynamometer for measuring propeller thrust and torque (Figure 3). The propellers were run at a speed of advance ( $V_A$ ) varying from 3.0 to 12.0 ft/sec and a rotational speed (N) from 7.0 to 11.0 revolutions per second permitting operation at Reynolds numbers  $R_n$  from 4.1 X 10<sup>5</sup> to 6.7 X 10<sup>5</sup>.

Since it was probable that various angular positions of the forward blades with respect to the aft blades would have an effect on the performance of the unit, the propellers were tested at two blade settings: the design setting (Setting 4), where the blades of the aft propellers were centered between those of the forward propeller (Figure 4), and Setting 1, where the blades of the two propellers were in line with each other (Figure 5).

## RESULTS

The comparison of the open water curves for Tandem Propellers 4148 and 4149 and parent Propeller 4118 are shown in Figure 6. Tabulated open water data for the tandem propellers at both blade settings are presented in Table 1. Both the tandem propellers and the parent propeller were

designed for uniform inflow for a K<sub>T</sub> near 0.15 at a speed coefficient, J, of 0.833. It can be seen from the performance characteristics shown in Table 2 that at the design angular spacing, the tandem propellers produced a higher thrust and torque than designed for but percentage wise were as near design as was the parent propeller. Overall, a peak efficiency of 75 percent is observed at a J of 0.94 for setting 1 (tandem) and an efficiency of .737 at a J of 0.91 for setting 4 (tandem) while the peak efficiency of propeller 4118 was 72 percent at a J = 0.94.

### CONCLUSIONS AND RECOMMENDATIONS

Based on the design performance characteristics the tandem propellers appear to be a suitable substitute for the parent propeller. Further studies are recommended for tandem propellers to determine which aspects of the design of such propellers, such as relative angular and axial position of the individual propellers, have the greatest affect on the overall performance characteristics of the unit. Also, since one of the potential gains of tandem propellers is to reduce cavitation, cavitation tests for the existing propellers should be performed and compared with cavitation tests of the partent propeller.

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η         J         KT         10Kq         ηο           .057         .050         .468         .702         .053           .112         .100         .454         .66         .106           .112         .100         .454         .66         .106           .217         .200         .422         .64         .288           .267         .250         .404         .622         .289           .316         .320         .386         .559         .388           .363         .350         .367         .559         .308           .409         .409         .347         .548         .404           .409         .450         .347         .548         .404           .409         .450         .347         .548         .404           .453         .550         .384         .463         .536           .575         .650         .284         .463         .536           .575         .650         .284         .404         .708           .678         .778         .780         .784         .708           .744         .900         .145         .270         .734	H	SETTING 1		SETTING 4	(DESIGN)	
150 .468 .702 150 .438 .64. 220 .438 .64. 350 .386 .599 350 .387 .574 400 .347 .578 400 .327 .521 500 .239 .402 550 .284 .463 650 .239 .402 700 .239 .304 850 .193 .337 1000 .073 .165 1100 .026 .094 1155 .000 .058	10Kq	η°			10KQ	700
100 454 6.  150 438 6.  200 462 64.  300 386 599  350 367 574  400 347 551  500 305 492  500 262 622  650 262 64.  750 305 492  750 193 337  800 121 236  1000 0073 165  1150 006 0054  1155 0.000 056	.632	• 05			702	.053
150	•618	==			. 9	106
250	•603	.16			17	.157
250 404 622 300 386 599 350 367 574 400 347 551 550 367 652 550 284 463 650 285 433 650 239 402 750 193 337 800 189 304 850 189 304 1000 0073 165 1150 006 008	.588	.21			. *9	.208
350 386 599 350 367 574 400 347 558 550 365 521 550 284 463 650 284 463 650 289 700 284 402 750 193 370 750 1121 236 1000 0073 1165 11150 002 0058	.572	•26			622	•520
350 367 574 400 347 558 450 327 551 500 284 492 550 284 492 650 289 402 700 239 402 750 193 337 850 145 270 1000 073 165 1100 026 098 1155 0.000 058	•555	.31			665	.30B
400 450 327 521 500 305 492 500 284 402 500 239 402 700 216 370 700 193 337 850 169 304 850 121 1000 1010	•538	•36			574	•356
450 327 521 500 305 492 550 284 463 600 262 433 650 239 402 700 216 370 700 193 337 850 169 304 850 169 304 1000 073 165 1100 026 094 1150 000 058	•520	04.			548	<b>*04</b>
550 305 492 550 284 463 600 262 433 650 239 402 700 216 370 750 193 337 850 169 304 850 169 304 1 000 073 165 1 100 026 094 1 155 0.000 058	•501	.45			521	6440
.550 .284 .463 .600 .262 .433 .650 .239 .402 .700 .216 .370 .750 .193 .337 .800 .169 .304 .850 .145 .270 .950 .097 .201 .1000 .073 .165 .1100 .026 .094 .1150 .002 .058	.480	64.			765	764.
.600 .262 .433 .650 .239 .402 .700 .216 .370 .750 .193 .337 .800 .169 .304 .950 .097 .201 .1000 .073 .165 .1100 .026 .094 .1155 0.000 .058	•458	•53			463	•536
.650 .239 .402 .700 .216 .370 .750 .193 .337 .800 .169 .304 .950 .145 .270 .950 .097 .201 1.000 .073 .165 1.100 .026 .094 1.155 0.000 .058	•435	.57			433	.577
750 .216 .370 .750 .193 .337 .800 .169 .304 .850 .145 .270 .950 .097 .201 1.000 .073 .165 1.150 .026 .094 1.155 0.000 .058	.410	.61			705	.615
. 750 . 193 . 337 . 800 . 169 . 304 . 304 . 304 . 304 . 304 . 304 . 306 . 950 . 097 . 201 . 100 . 026 . 094 . 1155 . 0.000 . 058 . 058	•384	•64			370	•650
.800 .169 .304 .850 .145 .270 .900 .121 .236 .950 .097 .201 1.050 .073 .165 1.100 .026 .094 1.150 .002 .058	•355	.67			337	.682
.850 .145 .270 .900 .121 .236 .950 .097 .201 1.000 .073 .165 1.100 .026 .094 1.150 .002 .058	•325	.70			304	.708
900 121 236 950 097 201 1.000 073 165 1.050 049 130 1.100 026 094 1.155 0.000 058	•293	.72			270	.727
1.050 .097 .201 1.000 .073 .165 1.050 .049 .130 1.100 .026 .094 1.150 .002 .058	•528	.74			236	.737
1.000 .073 .165 1.050 .049 .130 1.100 .026 .094 1.150 .002 .058	•225	.74			201	.733
1.050 .049 .130 1.100 .026 .094 1.150 .002 .058 1.155 0.000 .054 0	.183	.73	-		165	.706
1.150 .026 .094 1.150 .002 .058 1.155 0.000 .054 0.	.141	.67	1		130	.637
1.150 .002 .058 . 1.155 0.000 .054 0.	260.	.52	1		760	.480
0.000 .054 0.	•020	0.00	1		058	.068
			1.19	•	054	00000

Table 1 - Faired Values of Open Water Data for Two Settings of Propellers 4148-49

Propeller Number	Coefficient	Design	Open Water	Pct. Difference
4118	J	0.833	0.833	0
	K <sub>T</sub>	0.154	0.150	-3
	10K <sub>Q</sub>	0.290	0.285	-2
	ηο	0.706	0.698	-1
4148-49	J		0.833	
Setting 1	K <sub>T</sub>		0.166	
	10K <sub>Q</sub>	1	0.305	
	η,		0.723	
4148-4 <u>9</u>	J	0.833	0.833	0
Setting 4	K <sub>T</sub>	0.150	0.154	+3
	10K <sub>0</sub>	0.275	0.281	+2
	$\eta_{o}$	0.723	0.722	0

Table 2 - Open Water Performance at Design Advance Speed

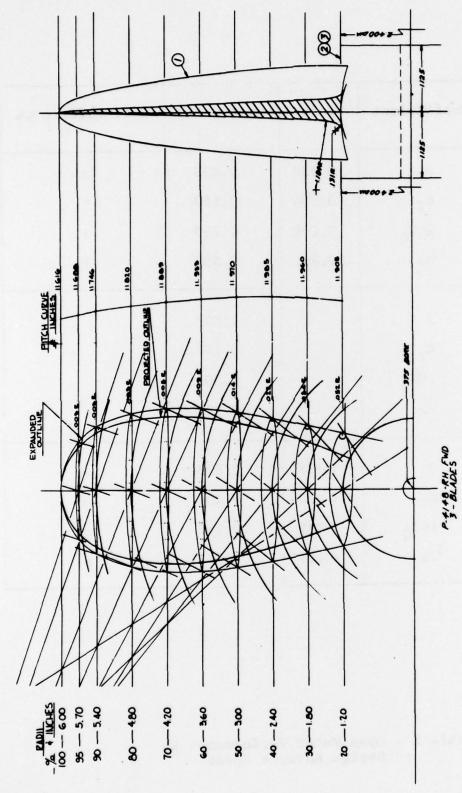


Figure 1 - Drawing of Propeller 4148 (Fwd)

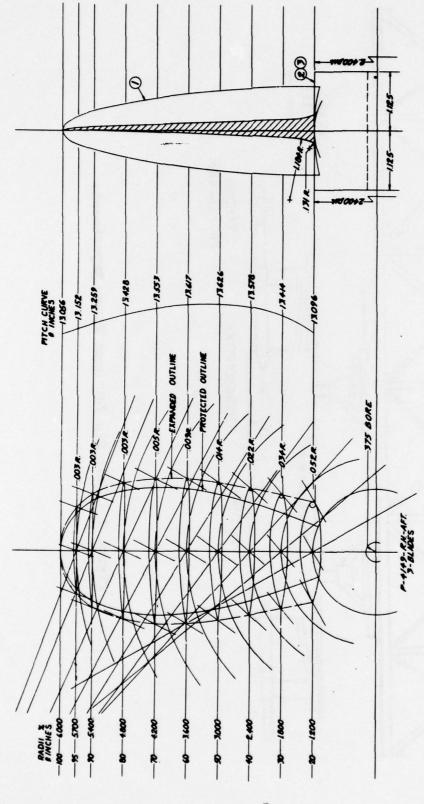


Figure 2 - Drawing of Propeller 4149 (Aft)

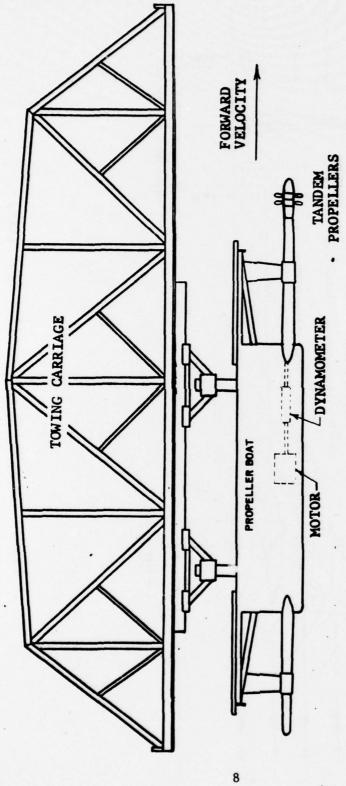


Figure 3 - Test Rig for Open Water Experiments

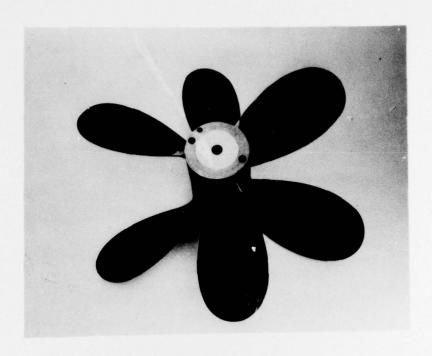
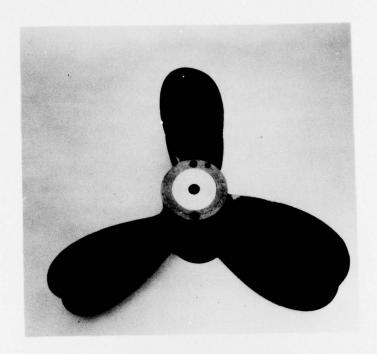




Figure 4 - Photographs of Propellers 4148-49 at Setting 4 (Design Setting)



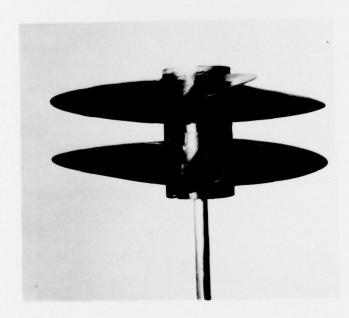


Figure 5 - Photographs of Propellers 4148-49 at Setting 1

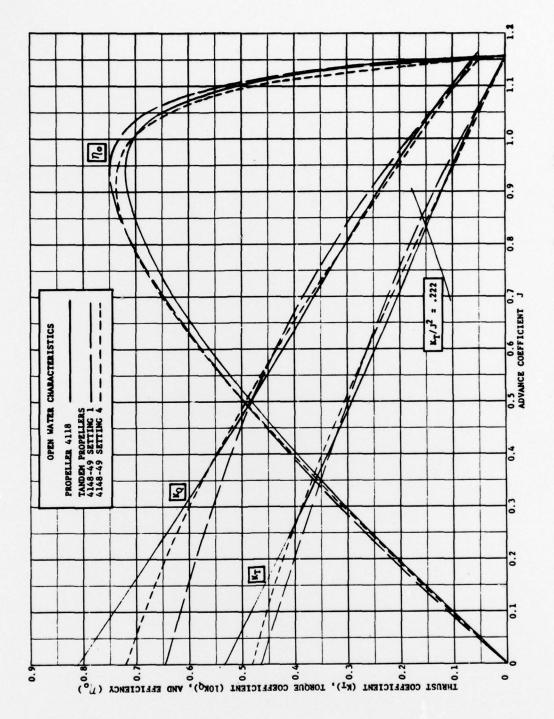


Figure 6 - Open Water Characteristics for Propellers 4148-49 and 4118

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